

Corrosion of reinforced concrete

I- Introduction

During its lifetime, the metallic structure of a building is attacked by the environment, especially by CO₂. Indeed, the iron is stable in basic media inside the concrete (pH = 12-14), but carbonates, dissolved in water, migrate through the concrete to the metallic part. This phenomenon implies a decrease of the pH localized around the metallic structure. This pH shift is represented by an arrow in the Pourbaix diagram [1] in Fig. 1. Then, at this acidic pH, the iron is no longer in its passive form but in its corrosive form. Consequently, the strength of the building is affected. For instance, the “Tour Perret” in Grenoble (Fig. 2), which is the first edifice built in reinforced concrete in Europe in 1924, is currently falling apart because of this process.

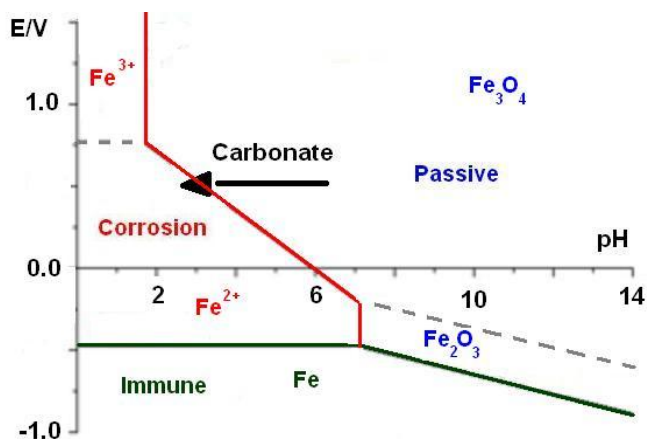


Fig. 1: Pourbaix diagram of iron [1].

In this context, an electrochemical process was developed to keep the neighborhood of the metallic rod in reinforced concrete in basic conditions [2-7]. For that, the materials to treat, which is a cathode, is immersed into a basic electrolytic paste (K₂CO₃ or Na₂CO₃) with an anode inserted in this paste (Fig. 3). The reduction of the water carried out at the metallic rod makes the media around the metallic rod more basic by production of OH⁻ (Eq. 1).

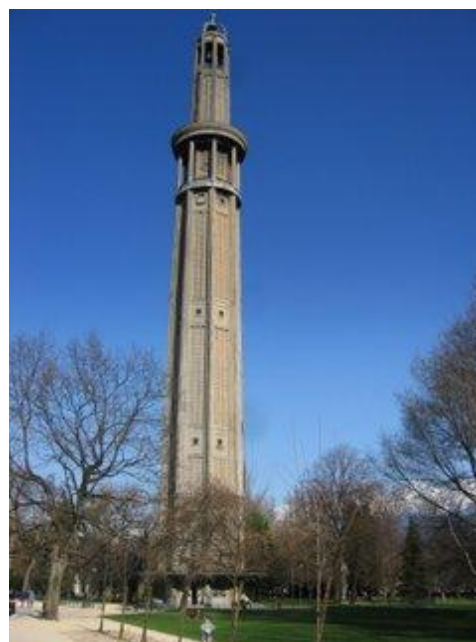
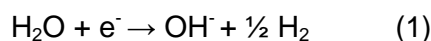


Fig. 2: The first edifice in reinforced concrete: the “Tour Perret” in Grenoble.

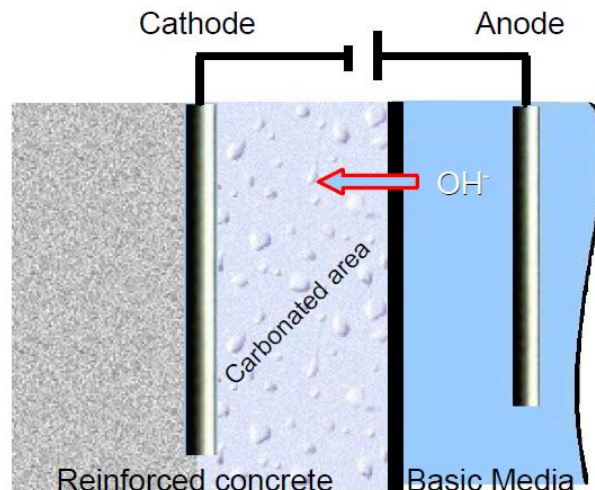


Fig. 3: Scheme of realkalisation method.

In this note, the corrosion process of the metallic rod in a concrete block is investigated. Realkalisation (electrolysis in basic media) is performed, and the benefits of the treatment are checked by Cyclic Potentiodynamic Polarization (CPP).

II-Experimental conditions

Investigations are carried out with the VMP3 instrument driven by EC-Lab® software in NaCl (3%) or NaOH solution (0.4 mol.L⁻¹). The concrete block is immersed for two days into the solution before measurements.

A three-electrode set-up is used:

- steel rod inside the concrete block as a working electrode with a surface area: $A = 10 \text{ cm}^2$ (Fig. 4),
- Ag/AgCl electrode as reference electrode,
- alloy wire as the counter electrode.

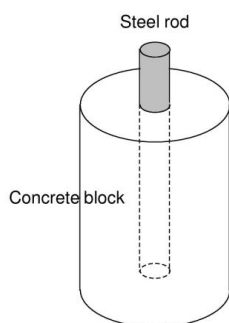


Fig. 4: Scheme of concrete reinforced block.

III- Results

III-1 Calculation of polarization resistance

First of all, we have to check if the material is under Tafel conditions [8,9]. For that, the resistance polarization (R_p) should be much higher than ohmic resistance (R_Ω). These two characteristics can be determined by electrochemical impedance spectroscopy (EIS) measurement (Fig. 5). The $R_\Omega = 202 \Omega$ is negligible versus $R_p > 12,800 \Omega$ (Fig. 6). Consequently, the conditions of « Tafel Fit » are respected.

R_p determination is also possible from voltamperometric measurements under a steady-state condition (very slow scan rate, *i.e.* 2.5 mV.min⁻¹) and in a narrow potential range ($\pm 10 \text{ mV}$ around the Open Circuit Voltage, *i.e.* -547 mV vs. Ag/AgCl). The voltamperogram and the « R_p Fit » are displayed in Fig. 7 and give $R_p = 11,744 \Omega$.

The R_p values determined by both methods are in agreement with each other.

It is possible to load the settings and the data files as PEIS_concrete_in_NaCl.mpr and MP_concrete_in_NaCl.mpr in the EC-Lab® Samples folder.

The screenshot shows the 'Parameters Settings' window of the EC-Lab software. Key parameters include:

- Mode:** Single Sine (selected), Multi Sine.
- Set E_{we} to E :** 0.0000 V vs. E_{oc} .
- for t_E :** 0 h 0 mn 0.000 s.
- Record every dI :** 0.000 mA or dt : 0.000 s.
- Scan from f_i :** 500 kHz to f_f : 0.170 Hz.
- with:** N_d = 5 points per decade (selected), or N_T = 51 points from f_i to f_f .
- in:** Logarithmic spacing (selected), or Linear spacing.
- sinus amplitude V_a :** 10.0 mV ($V_{rms} \sim 7.07 \text{ mV}$).
- wait for p_w :** 0.00 period before each frequency.
- average N_a :** 1 measure(s) per frequency.
- drift correction:** unchecked.
- Repeat n_c :** 0 time(s).
- E Range:** -10 V; 10 V. Resolution = 305.18 μV .
- I Range:** Auto.
- Bandwidth:** 5 - medium (~ 27 s / scan).
- Go back to seq. N_s :** 0 (SSS ends technique).
- for n_r :** 0 time(s) (0 for next sequence).
- increment cycle number:** unchecked.

Fig. 5: “Parameters Settings” window of potentiostatic electrochemical impedance spectroscopy measurements (PEIS) performed in NaCl (3%).

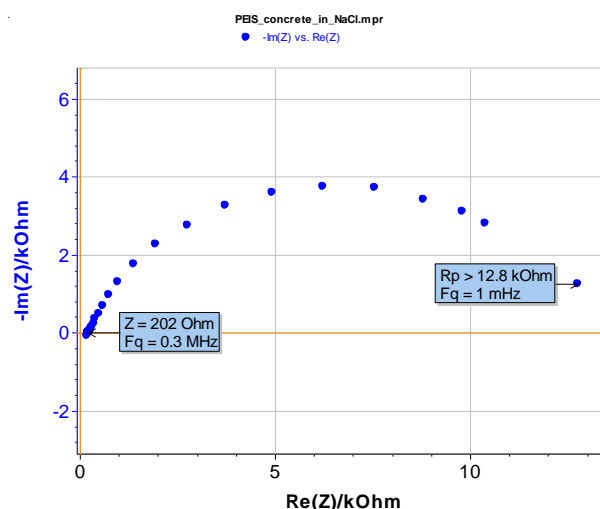


Fig. 6: Nyquist diagram of concrete block.

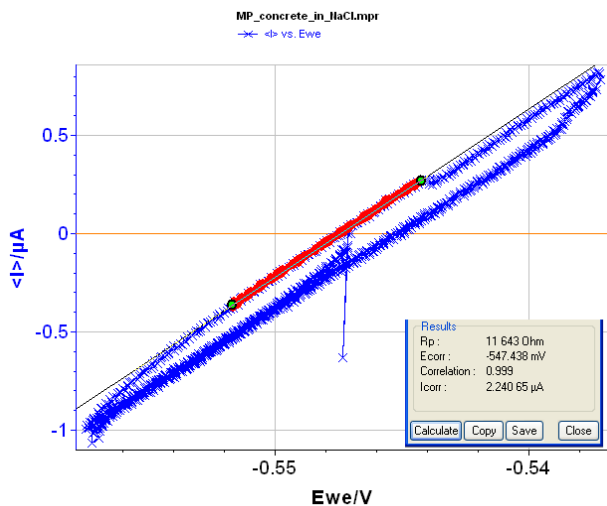


Fig. 7: Voltamperogram and “R_p Fit” of the block in NaCl (3%).

III-2 Realkalisation

Realkalisation treatment is performed with the chronopotentiometric (CP) techniques in NaOH (0.4 mol.L⁻¹; pH = 13) for 66 h (Fig. 8) at $I_s = -10$ mA. Potential and charge during the electrolysis are plotted in Fig. 9. At the end of the electrolysis, a stable potential of -2.4 V vs. Ag/AgCl is reached.

III-3-Characterizations of the metallic rod.

In order to check the efficiency of the realkalisation, CPP experiments are carried out before and after the treatment. The parameters of these experiments are given in Fig. 10.

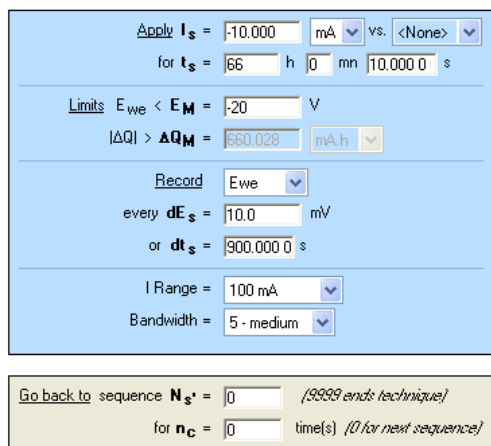


Fig. 8: “Parameters Settings” Window of chronopotentiometry (CP).

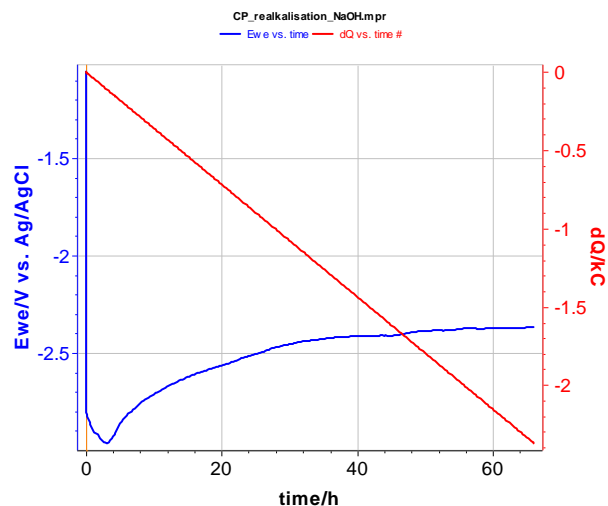


Fig. 9: Plot of potential (blue curve) and charge (red curve) during the electrolysis .

It is possible to load the settings and the data files as CP_Realkalisation_NaOH.mpr in the EC-Lab[®] Samples folder.

A comparison between CPP before and after realkalisation (Fig. 11) displays a cathodic shift due to steel rod reduction. “Tafel Fit” analysis is performed for both curves and gives $E_{corr} = -616$ and -1077 mV vs. Ag/AgCl for the CPP measurement performed before and after treatment, respectively.

Other parameters (I_{corr} , β_c , β_a , and corrosion rate) are computed (Fig. 11 and Table 1). The corrosion rate is given by Eq. 2:

$$CR = I_{corr} K EW / (d A) \quad (2)$$

in which K is a constant, EW is the equivalent weight, d is the density, and A is the surface area of the electrode. In the case of steel, EW and d are 18.616 g/eq. and 7.8, respectively.

These fits show that corrosion rate is 50% higher before than after realkalisation. This decrease of the corrosion rate demonstrates the efficiency of the realkalisation process.

Rest for t_R = 0 h 0 min 0 s
 Limit $|dE_{we}/dt| < dE_R/dt$ = 0.0 mV/h
 Record every dE_R = 0.0 mV
 or dt_R = 500 s

Scan E_{we} with dE/dt = 5 mV/s
 from E_i = -1.3 V vs. Ref
 to E_L = 1.300 V vs. Ref

Limit $|I| > I_P$ = 100.000 mA after t_b
 t_b = 0.1000 s from scan beginning

Record <I>
 over the last 25 % of the step duration
 average N = 3 voltage steps

E Range = -10 V; 10 V
 Resolution = 305.18 μV

I Range = Auto
 Bandwidth = 5 - medium

Hold E_L Until $|I| > I_P$ (if I limit not previously reached)

End scan to E_f = -1.300 V vs. Ref
 Limit $|I| < I_f$ = 0.000 μA

($dE/dt \sim 300 \mu V / 60.0 ms$)
 ($dEN \sim 900 \mu V$)

Fig. 10: "Parameters Settings" Window of CPP experiments.

It is possible to load the settings and the data files as CPP_Before_Realkalisation.mpr and CPP_After_Realkalisation.mpr in the EC-Lab® Samples folder.

Table 1: Data from CPP investigations.

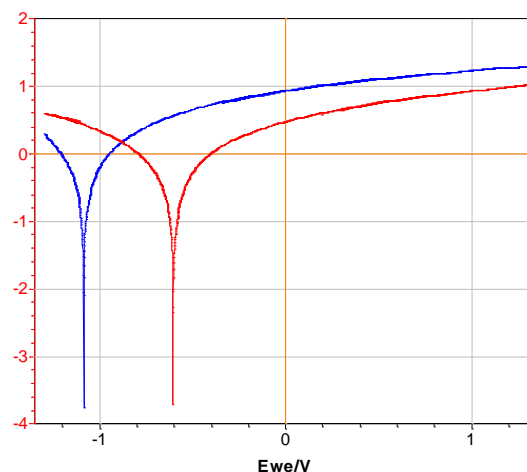
	Before	After
E_{corr}/mV vs. Ag/AgCl	-616	-1097
$I_{corr}/\mu A$	404	272
β_c/mV vs. Ag/AgCl	646	240
β_a/mV vs. Ag/AgCl	670	325
Corrosion rate/mmpy*	0.315	0.213

*mmpy: mm per year

IV- Conclusion

This note demonstrates that electrochemical techniques are able to recondition (electrolysis) and characterize (CPP, impedance, and their corresponding analysis) the metallic structure of buildings.

It is an example of the contribution of the electrochemistry to the field of civil engineering.



Before

After

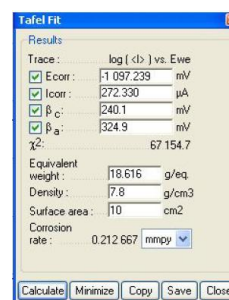
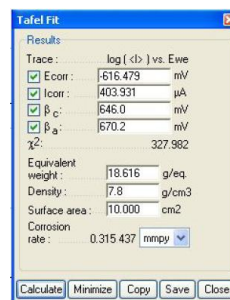


Fig. 11: Evans diagram of the reinforced concrete before (in red) and after (in blue) realkalisation (top) and "Tafel Fit" results (bottom).

References

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